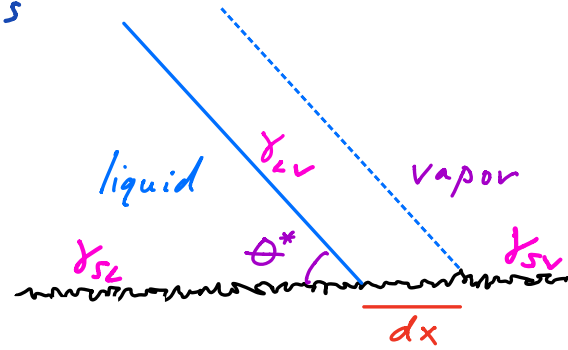


# Lecture 16. Wetting of rough solids; coating flows

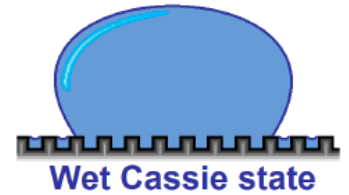
Effective contact angle  $\theta^*$  depends on both chemistry (which sets  $\theta_e$ ) and roughness parameters

$$r = \frac{\text{TOTAL SURFACE AREA}}{\text{PROJECTED AREA}}$$

$$\phi_s = \frac{\text{AREA OF ISLANDS}}{\text{PROJECTED AREA}}$$



For drops on rough solids, there are 3 possible states:



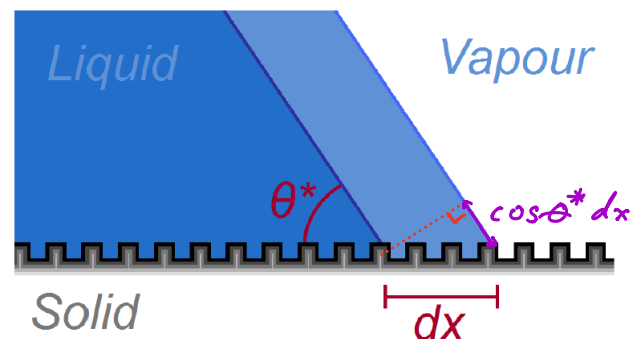
## Wenzel Model (1936)

Change in wetting energy :

$$dE_w = r (\gamma_{sl} - \gamma_{sv}) dx$$

$$+ \gamma \cos \theta^* dx$$

NEW INTERFACE



If  $r = 1$  (smooth surface):  $\Rightarrow$  retain Young's Law

$$\text{If } r > 1 : \cos \theta^* = r \cos \theta_e$$

$\Rightarrow$  wetting/nonwetting tendencies amplified by roughness  
e.g. a hydrophobic surface may become superhydrophobic

in respond to roughening

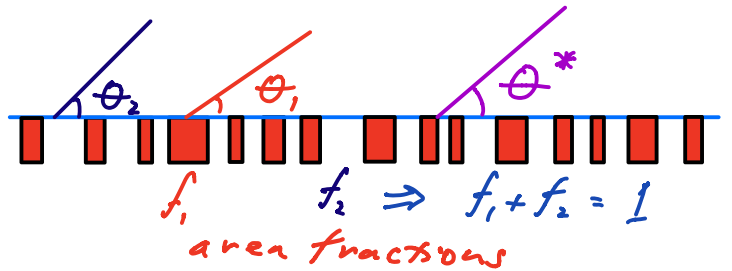
Note: for  $\theta_e < \theta_c$  (depends on texture)

$\Rightarrow$  demi-wicking, complete wetting  
 $\Rightarrow$  Wet Cassie state

Restriction of Wenzel Model: for  $\theta_e > \frac{\pi}{2}$ , breaks down at large  $r$ , when air is trapped in inclusions

Cassie-Baxter Model: applies to wetting on a planar but chemically heterogeneous surface.

Consider surface with 2 species, one with area fraction  $f_1$  and equilibrium contact angle  $\theta_1$ , the other with  $f_2, \theta_2$ .



Energy Variation

$$dE = f_1(\gamma_{SL} - \gamma_{SV})_1 dx + f_2(\gamma_{SL} - \gamma_{SV})_2 dx + \gamma \cos \theta^* dx$$

Equilibrium when  $dE = 0$ :

$$\cos \theta^* = f_1 \cos \theta_1 + f_2 \cos \theta_2$$

Cassie-Baxter

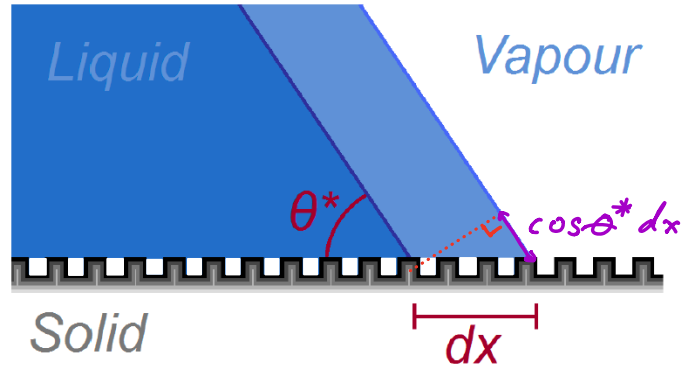


Consider 2 special cases ...

I. Hydrophobic ( $\theta_e > \frac{\pi}{2}$ ,  $\cos \theta_e < 0$ )

$\Rightarrow$  Dry Cassie State

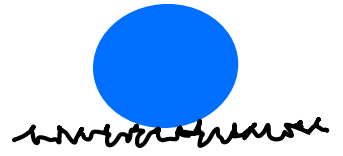
• the 2 phases are the solid ( $\theta_1 = \theta_e$ ,  $f_1 = \phi_s$ ) and air ( $\theta_2 = \pi$ ,  $f_2 = 1 - \phi_s$ ), so we have:



$$\cos \theta^* = \phi_s \cos \theta_e - 1 + \phi_s$$

Note: 1. as pillar density  $\phi_s \rightarrow 0$ ,  $\cos \theta^* \rightarrow -1$ ,  $\theta^* \rightarrow \pi$

2. drops in the dry Cassie state are said to be in the "Fakir state"



3. contact angle hysteresis greatly increased in Wenzel state, decreased in Cassie

4. maintenance of Cassie state is key for water repellency

5. Cross-over between Wenzel and Dry Cassie States

Wenzel state preferable when

$$dE_w < dE_c$$

$$\text{i.e. } -v \cos \theta_c + \cancel{\cos \theta^*} < -\phi_s \cos \theta_e + (1 - \phi_s) + \cancel{\cos \theta^*}$$

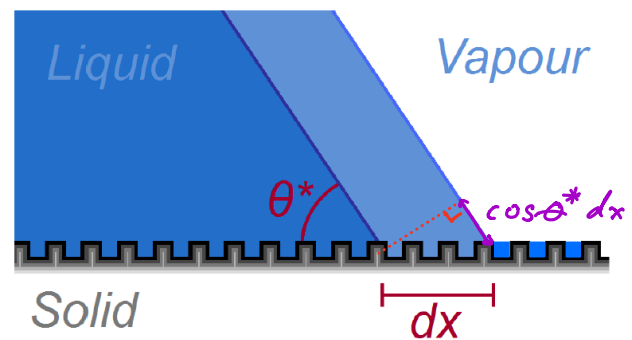
$$\text{i.e. } \boxed{\cos \theta_e > \frac{-1 + \phi_s}{v - \phi_s}} = \cos \theta_c^* = -\cos \theta_c$$

## II. Hydrophilic case ( $\theta_e < \theta_c$ ): Wet Cassie

- here, the Cassie state corresponds to a tiled surface with 2 phases, the solid ( $\theta_1 = \theta_e, f_1 = \phi_s$ ) and the liquid ( $\theta_2 = 0, f_2 = 1 - \phi_s$ )

Subbing into  $\star$ :

$$\boxed{\cos \theta^* = 1 - \phi_s + \phi_s \cos \theta_e}$$



The critical transition value of  $\theta_c$  between Wenzel and Wet Cassie states may be deduced by equating energies in these 2 states:

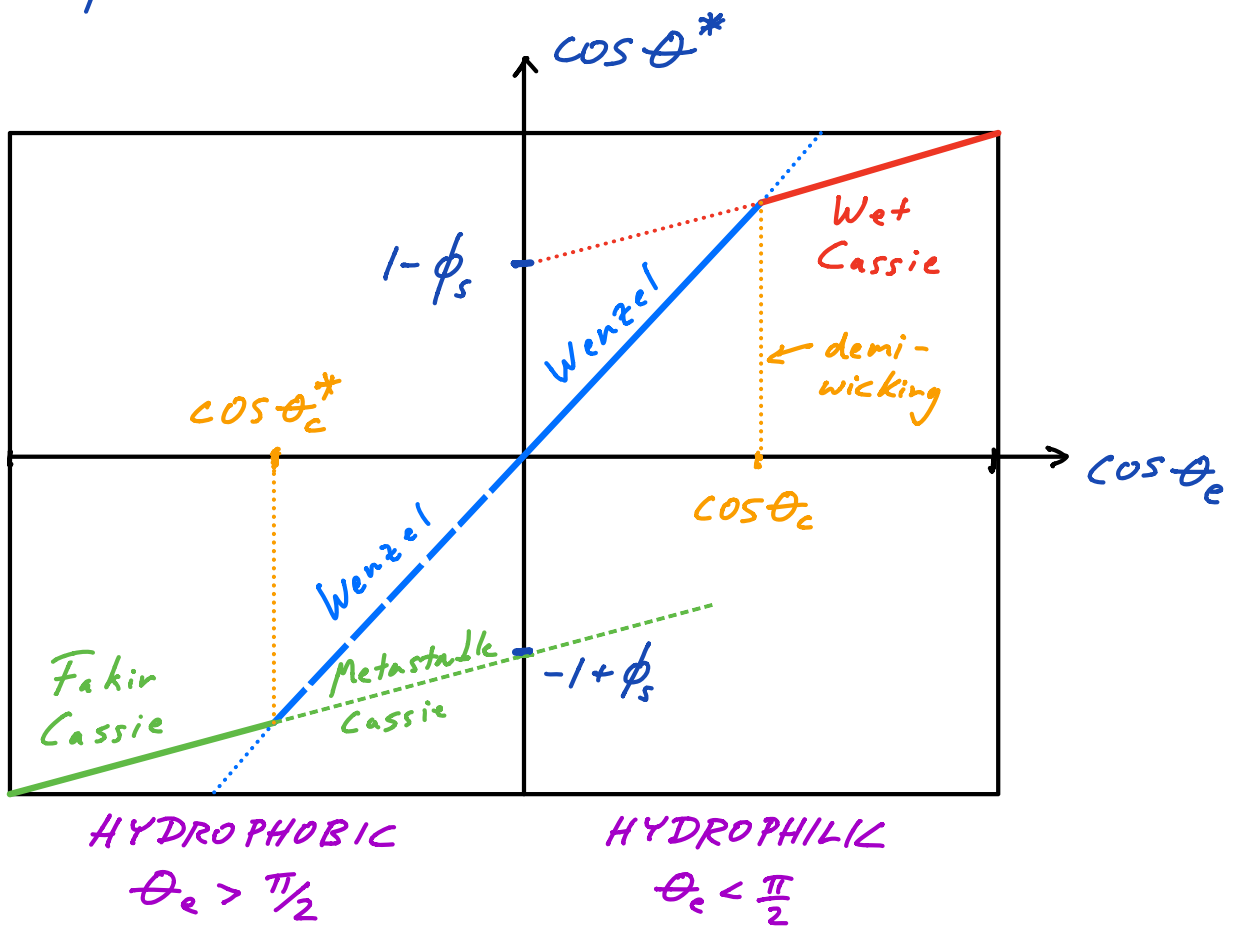
$$v \cos \theta_e = 1 - \phi_s + \phi_s \cos \theta_e \Rightarrow \theta_e = \theta_c$$

and corresponds to condition for demi-wicking

$\Rightarrow$  when  $\frac{\pi}{2} > \theta_e > \theta_c$ , solid remains dry ahead of the drop  $\Rightarrow$  Wenzel

$\Rightarrow$  when  $\theta_e < \theta_c \Rightarrow$  liquid penetrates texture  $\Rightarrow$  Wet Cassie

# Summary



Note differences between hydrophobic + hydrophilic regimes.

Hydrophilic: Wenzel's Law ceases to apply at small  $\theta_e$ , when demi-wicking sets in  $\Rightarrow$  Wet Cassie states

Hydrophobic: one may see a discontinuous jump in  $\theta^*$  as  $\theta_e$  increases due to hysteresis, the existence of a metastable Cassie state

- jump largest for large roughness (small  $\phi_s$ )

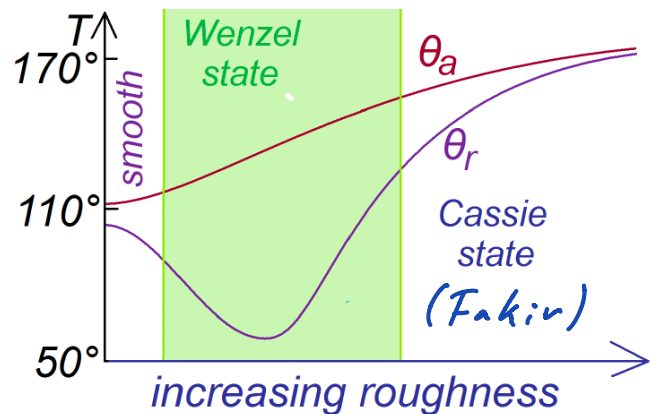
# Historical Notes

1. Early studies of wetting motivated by insecticides
2. Chemists have since been trying to design hydrophobic (or oleophobic) surfaces using a combination of chemistry + texture
3. recent advances in micro-fabrication have achieved

$$\theta^* \approx \pi, \quad \Delta\theta = 0.$$

## 4. Johnson + Dettre (1964)

- o examined water drops on wax, whose roughness was controlled with temperature
- ⇒ showed increase, then decrease of  $\Delta\theta = \theta_a - \theta_r$  as roughness increased: smooth → Wenzel → Cassie (Fakir)



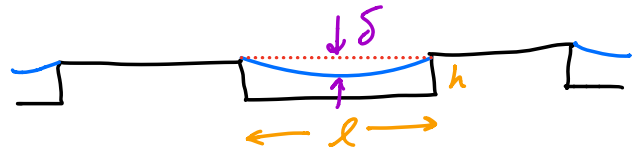
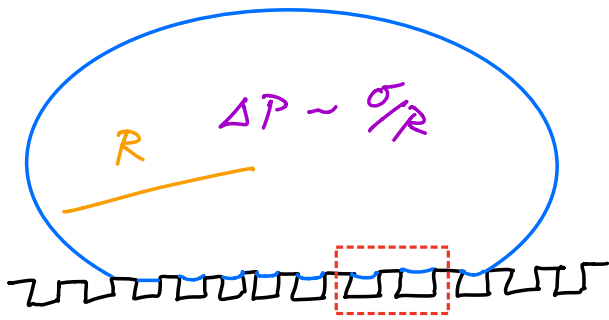
## Water-repellency

- o requires the maintenance of a Dry Cassie state  
i.e. impregnation pressure must be exceeded by Laplace pressure induced by roughness

## Eq. 1 Static drop

Pressure jump across its surface:  $\frac{\sigma}{R} \approx \sigma \frac{\delta}{l^2}$

Interface will touch down if  $\delta > h$ .

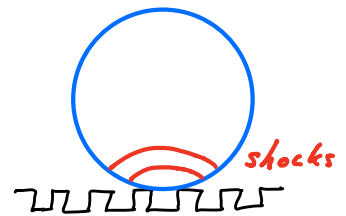


ie.  $R < \frac{l^2}{h} \Rightarrow$  longer pillars are more hydrophobic

## Eg. 2 Impacting Drop

$$\Delta P \sim \rho V^2 \text{ or } \rho V c$$

↑  
Speed of sound



## Eg. 3 Submerged surface e.g. on side of boat or diving insect

Impregnation pressure

$$\Delta P = \rho g z$$

