

Lecture 12: Instability of a fiber coating; Film retraction

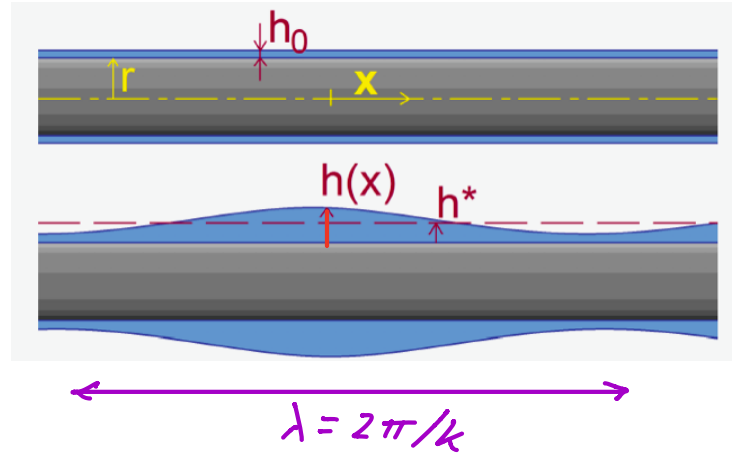
Instability of a fluid coating on a fiber

Define mean thickness:

$$h^* = \int_0^1 h(x) dx$$

so interface thickness

$$h = h^* + \Sigma \cos kx$$



Continuity: $\int_0^1 \pi (r+h)^2 dx = \int_0^1 \pi (r+h_0)^2 dx$

$$\Rightarrow \int_0^1 (r+h^* + \Sigma \cos kx)^2 dx = (r+h_0)^2 \cdot 1$$

$$\int_0^1 (r+h^*)^2 + \Sigma^2 \cos^2 kx + 2(r+h^*) \Sigma \cos kx dx = (r+h_0)^2 \cdot 1$$

$$\Rightarrow (r+h^*)^2 \cdot 1 + \Sigma^2 \cdot \frac{1}{2} + 0 = (r+h_0)^2 \cdot 1$$

$$\Rightarrow (r+h^*)^2 = (r+h_0)^2 \left[1 - \frac{1}{2} \frac{\Sigma^2}{(r+h_0)^2} \right]$$

$$\Rightarrow h^* = h_0 - \frac{1}{4} \frac{\Sigma^2}{r+h_0} \quad \boxtimes$$

So, when does perturbation reduce surface energy?

i.e. when is $\int_0^1 2\pi (r+h) ds < 2\pi (r+h_0) \cdot 1$?

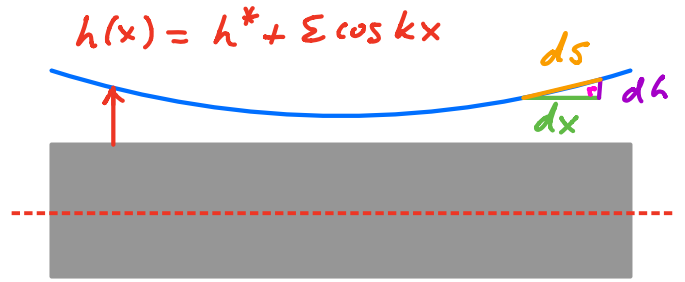


Note: $ds^2 = dh^2 + dx^2$

$$\Rightarrow ds = dx \left[1 + \left(\frac{dh}{dx} \right)^2 \right]^{\frac{1}{2}}$$

$$\approx dx \left[1 + \frac{1}{2} \varepsilon^2 k^2 \sin^2 kx \right]$$

since $\frac{dh}{dx} = -\varepsilon k \sin kx$



$$\begin{aligned} \Rightarrow \int_0^\lambda (v+h) ds &= \int_0^\lambda (v+h^* + \varepsilon \cos kx) \left(1 + \frac{1}{2} \varepsilon^2 k^2 \sin^2 kx \right) dx \\ &= (v+h^*)\lambda + \frac{1}{4} (v+h^*) \varepsilon^2 k^2 \lambda + O(\varepsilon^3) \end{aligned}$$

So, \star holds provided:

$$(v+h^*)\lambda + \frac{1}{4} (v+h^*) \varepsilon^2 k^2 \lambda < (v+h_0)\lambda$$

Sub in $(h^* - h_0)$ from \boxtimes :

$$-\frac{1}{4} \frac{\varepsilon^2}{v+h_0} + \frac{1}{4} (v+h^*) \varepsilon^2 k^2 < 0$$

Result indep of ε : $k^2 < (v+h_0)^{-1} (v+h^*)^{-1}$
 $\approx \frac{1}{(v+h_0)^2}$

i.e. wavelength

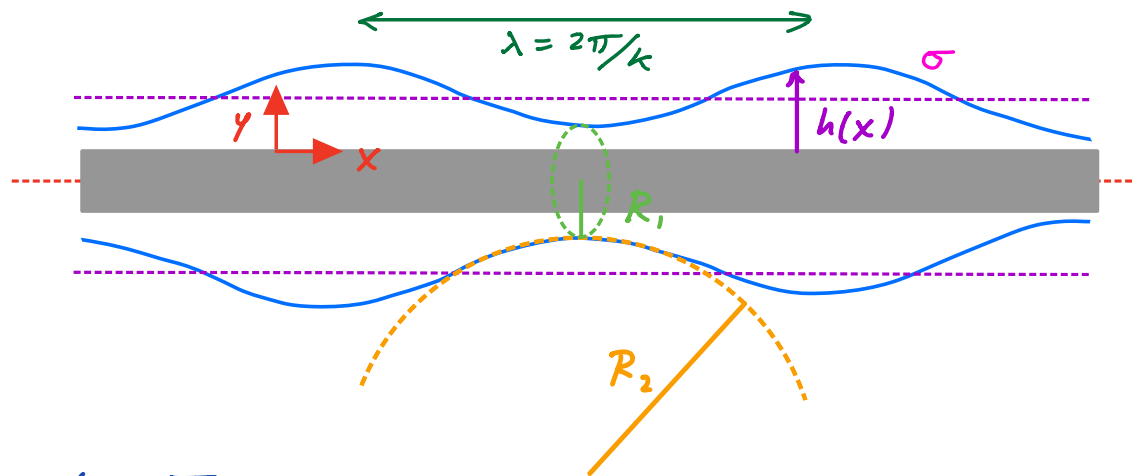
$$\lambda = \frac{2\pi}{k} > 2\pi (v+h_0)$$

\Rightarrow comparable to standard Ra-P.

All long λ will grow, but which grows fastest?

\Rightarrow determined by dynamics, not just geometry.

Consider dynamics in the thin-film limit,
 $h_0 \ll \nu \Rightarrow$ LUBRICATION THEORY.



Dynamics of Instability (Rayleigh 1879)

Poiseuille flow (Couette):

$$\eta \frac{d^2 v}{dy^2} - \frac{dp}{dx} = 0$$

↳ GRADIENT IN CURVATURE PRESSURE,
 INDEP of y .

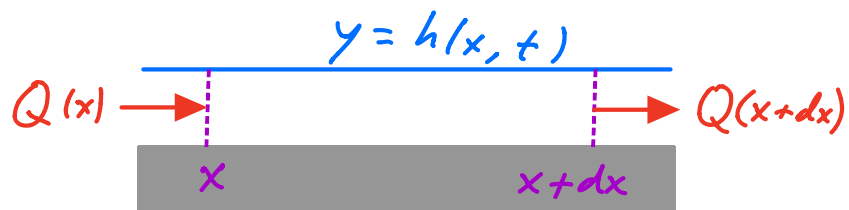
$$\Rightarrow \frac{dv}{dy} = \frac{1}{\eta} \frac{dp}{dx} (y - h)$$

$$v(y) = \frac{1}{2\eta} \frac{dp}{dx} \left(\frac{y^2}{2} - h y \right)$$

Flux: $Q_{/cm} = \int_0^h v(y) dy = -\frac{1}{3\eta} \frac{dp}{dx} h^3$

Lubrication: $Q(x+dx) - Q(x) = -\frac{dh}{dt} dx$

$$\begin{aligned} \Rightarrow \frac{dQ}{dx} &= -\frac{h_0^3}{3\eta} \frac{d^2 p}{dx^2} \\ &= -\frac{dh}{dt} \end{aligned}$$



Curvature pressure : $p(x) = \sigma \left(\frac{1}{R_1} + \frac{1}{R_2} \right)$
 $= \sigma \left(\frac{1}{r+h} - \frac{d^2 h}{dx^2} \right)$

$$\Rightarrow \frac{dh}{dt} = \frac{\sigma h_0^3}{3\eta} \frac{d^2}{dx^2} \left[\frac{1}{r+h(x)} - h_{xx} \right]$$

$$= \frac{\sigma h_0^3}{3\eta} \frac{d^2}{dx^2} \left[\frac{1}{r+h^*} - \frac{\Sigma \cos kx}{(h^*+r)^2} + \Sigma k^2 \cos kx \right]$$

since $h(x,t) = h^* + \Sigma(t) \cos kx$

$$h_x = -\Sigma k \sin kx, \quad h_{xx} = -\Sigma k^2 \cos kx$$

$$= -k^2 h$$

$$h_t = \cancel{h_t^*} + \frac{d\Sigma}{dt} \cos kx$$

$$\Rightarrow \cancel{\cos kx} \frac{d\Sigma}{dt} = \frac{\sigma h_0^3}{3\eta} \Sigma \cancel{\cos kx} \left[\frac{k^2}{(r+h^*)^2} - k^4 \right]$$

$$\therefore \frac{d\Sigma}{dt} = \beta \Sigma$$

DISPERSION RELATION

where $\beta = \frac{\sigma h_0^3}{3\eta} \left[\frac{k^2}{(r+h_0)^2} - k^4 \right]$

Recall: $h^* = h_0 - \frac{1}{4} \Sigma^2 \frac{1}{(r+h_0)^2} \approx h_0$

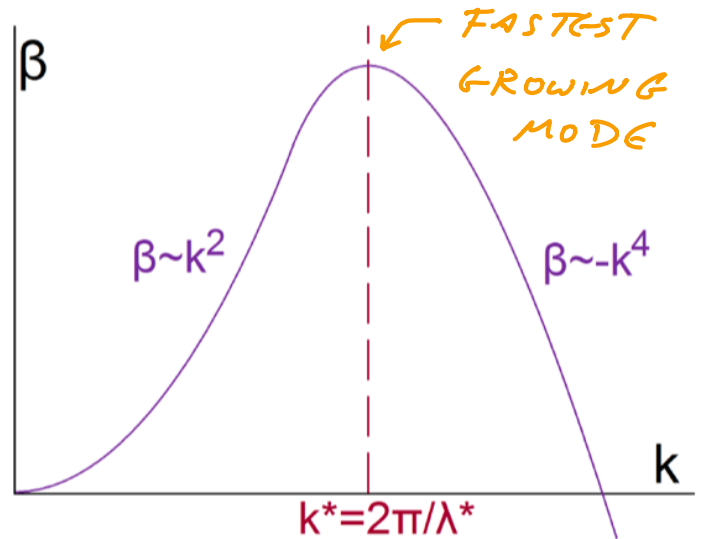
Fastest Growing Mode:

$$\text{Arises when } \frac{d\beta}{dk} = 0 = \frac{2k^*}{(r+h_0)^2} - 4k^{*3}$$

$$\Rightarrow \lambda^* = 2\pi\sqrt{2} (r+h_0)$$

$$\approx 10 (r+h_0)$$

similar to inviscid
Rayleigh - Plateau



We also see the timescale of instability :

$$\tau^* = \frac{2\pi}{\beta(k^*)} = \frac{12\eta(r+h_0)^4}{\sigma h_0^3} \quad \star$$

Scaling Argument for Pinch-off time?

$$\frac{\mu V}{h_0^2} \sim \underline{\nabla} p \sim \underline{\nabla} [\sigma \underline{\nabla} \cdot \underline{u}]$$

VISCOS STRESS
CURVATURE PRESSURE
 $\sim \frac{1}{r} \sigma \frac{h_0}{r^2}$

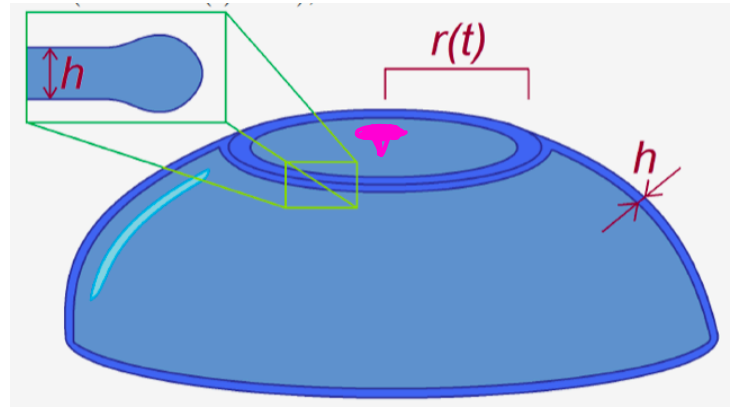
$$\Rightarrow V \sim \frac{V}{\tau_p} \sim \frac{\sigma}{\mu} \frac{h_0^3}{r^3}$$

$$\Rightarrow \tau_p \sim \frac{\mu}{\sigma} \frac{r^4}{h_0^3} \quad \Rightarrow \text{COMPARE TO COMPLETE RESULT} \quad \star$$

Rupture of a Soap Film (Culick 1960, Taylor 1960)

- neglect viscous effects, consider inviscid limit

Note: the force/length acting on the rim may be calculated via Frenet-Serret axis:

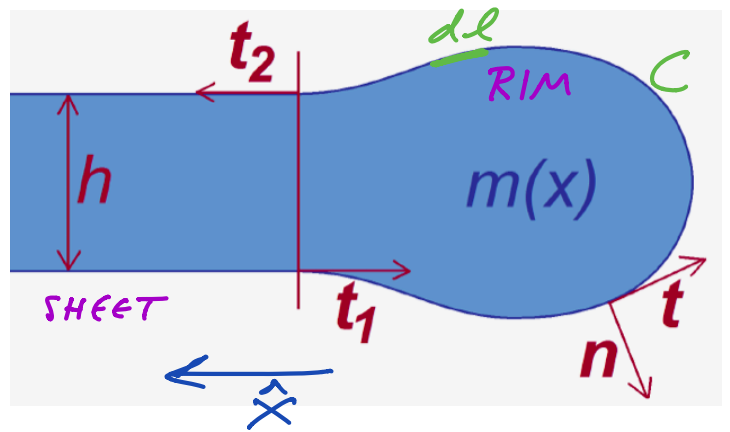


$$\underline{F}_c = \int_c \sigma \underline{\nabla} \cdot \underline{u} \underline{u} \, dl \quad \text{where } (\underline{\nabla} \cdot \underline{u}) \underline{u} = \frac{d\underline{t}}{dl}$$

$$= \int_c \sigma \frac{d\underline{t}}{dl} \, dl$$

$$= \sigma (\underline{t}_1 - \underline{t}_2)$$

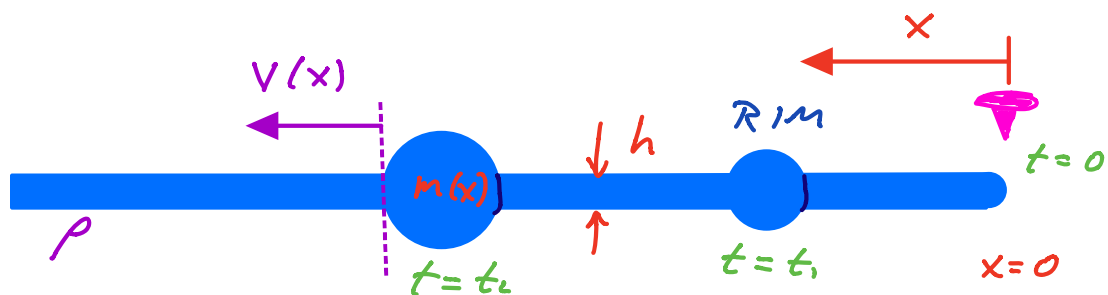
$$= 2\sigma \hat{x}$$



At time $t=0$, a planar sheet is punctured at $x=0$ and retracts in the \hat{x} -direction under the influence of $F_c = 2\sigma \hat{x}$.

Observation: rim engulfs the film

- no upstream disturbance



Rim mass : $m(x) = \rho h x$

Rim speed : $V = \frac{dx}{dt}$

Inertial force on rim = rate of change of rim momentum

$$\begin{aligned} F_I &= \frac{d}{dt} (mV) = V \frac{d}{dx} (mV) \\ &= V^2 \frac{dm}{dx} + mV \frac{dV}{dx} \\ &= \frac{1}{2} V^2 \rho h + \frac{1}{2} \frac{d}{dx} (mV^2) \end{aligned}$$

Force Balance : Curvature Force = Inertial Force

$$\Rightarrow 2\sigma = \frac{d}{dx} \left(\frac{1}{2} mV^2 \right) + \frac{1}{2} \rho h V^2$$

Integrating from 0 to x :

$$\int_0^x 2\sigma dx = \int_0^x d \left(\frac{1}{2} mV^2 \right) + \frac{1}{2} \rho h \int_0^x V^2 dx$$

$$2\sigma x = \frac{1}{2} \rho h x V^2 + \frac{1}{2} \rho h \int_0^x V^2 dx$$

SURFACE ENERGY
RELEASED/LENGTH

K.E. OF RIM

ENERGY REQUIRED
TO ACCELERATE RIM

Now assume V is indep of x (observed in lab),
so that

$$\int_0^x V^2 dx = x V^2$$

$$\Rightarrow 2\sigma x = \rho h x V^2$$

$$V = \left(\frac{2\sigma}{\rho h} \right)^{\frac{1}{2}}$$

Culick Speed of film retraction

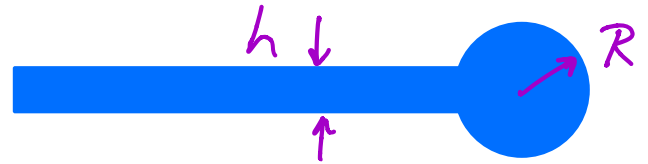
Note: 1. for a water/soap film of $h \sim 150 \mu\text{m}$

$\Rightarrow V \sim 3 \cdot 10^2 \text{ cm/s}$ very high

2. Surface area of rim/length: $P = 2\pi R$

where $m = \rho h x = \pi \rho R^2$

$$\Rightarrow R(x) = \sqrt{\frac{hx}{\pi}}$$



o Rim surface energy: $\sigma P = \sigma 2\pi \sqrt{\frac{hx}{2\pi}}$

Total surface energy: $\sigma [2x + 2(\pi hx)^{\frac{1}{2}}]$

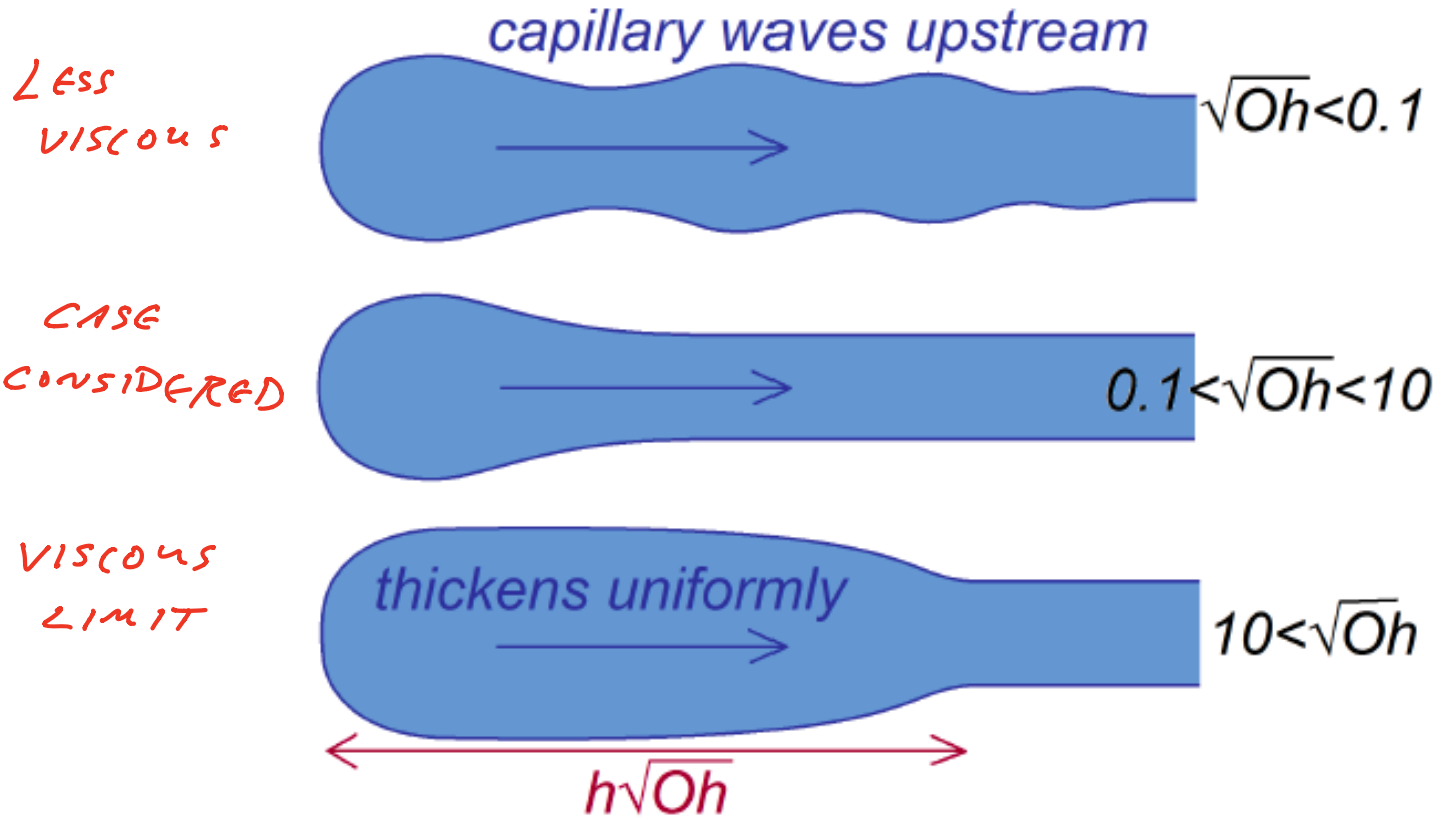
Scale: $\frac{SA_{\text{rim}}}{SA_{\text{sheet}}} \sim \frac{2\pi \sqrt{hx}}{2x} \sim \pi \left(\frac{h}{x} \right)^{\frac{1}{2}} \ll 1$
for $x \gg h$



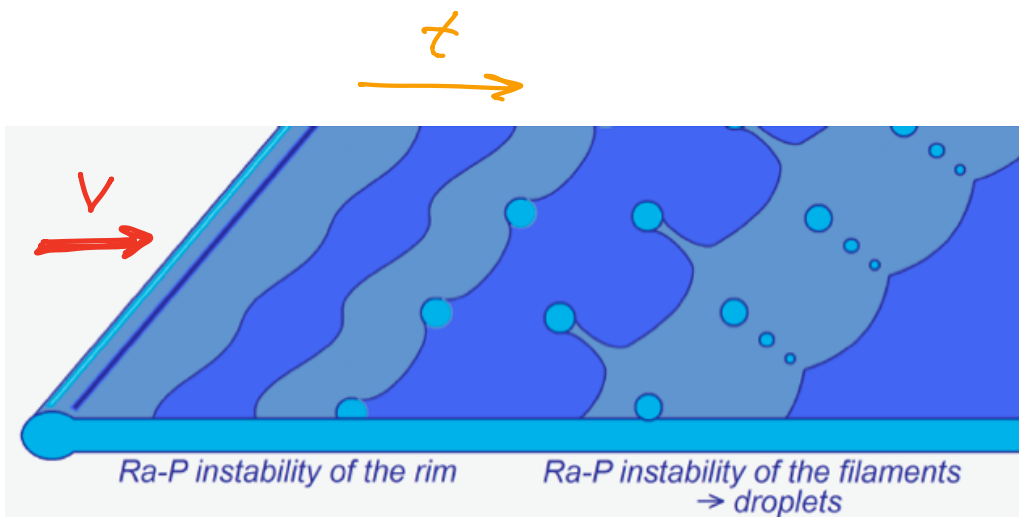
But, a circular film may self-heal if the hole is suff. small.

3. For dependence on geometry (ie. circular hole) and influence of viscosity, see Savva + Bush (JFM, 2009)

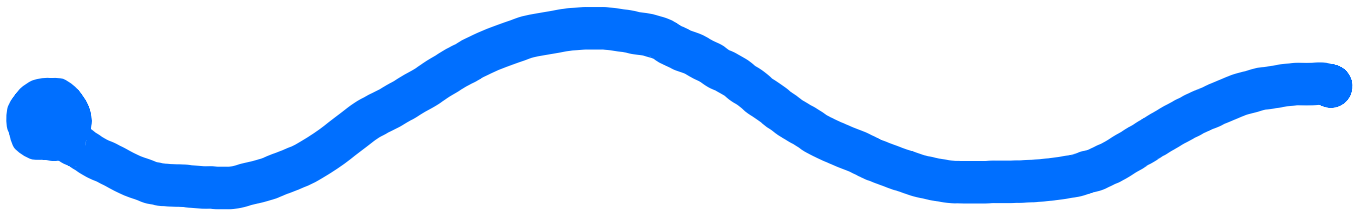
4. form of rim/sheet evolution depend on Ohnesorge # : $\sqrt{Oh} = \frac{\mu}{\sqrt{2h\rho\sigma}}$



5. The growing cylindrical rim is subject to Ra-P \Rightarrow often pinches into drop



6. At very high speed, shear stresses caused by air induce flapping.



⇒ like a flapping flag, with flag elasticity replaced by Merzingeri elasticity
[Lhuissier + Villermanx (PRL, 2009)]